

(19) World Intellectual Property Organization
International Bureau(43) International Publication Date
13 July 2006 (13.07.2006)

PCT

(10) International Publication Number
WO 2006/073712 A1

(51) International Patent Classification:

C08J 9/00 (2006.01) C08J 9/12 (2006.01)
C08K 3/04 (2006.01)

(21) International Application Number:

PCT/US2005/045291

(22) International Filing Date:

14 December 2005 (14.12.2005)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

11/026,011 31 December 2004 (31.12.2004) US

(71) Applicant (for all designated States except US): OWENS CORNING [US/US]; One Owens Corning Parkway, Toledo, Ohio 43659 (US).

(72) Inventors; and

(75) Inventors/Applicants (for US only): LOH, Roland, R. [US/US]; 2082 Darrow Lake Drive, Stow, Ohio 44224 (US). POLASKY, Mark, E. [US/US]; 1408 Countryside Drive, Mogadore, Ohio 44260 (US). RYND, Joseph, P. [US/US]; 2069 Forest Edge Drive, Cuyahoga Falls, Ohio 43223 (US). LEE, James, L. [US/US]; 1109 Millcreek Lane, Columbus, Ohio 43220 (US). HAN, Xiangmin [CN/US]; 618 Harley Drive, Apartment 1, Columbus, Ohio 43202 (US). KOELLING, Kurt, W. [US/US]; 8454 Daventry Court, Powell, Ohio 43065 (US).

(74) Agents: GASAWAY, Maria, C. et al.; Owens Corning Science & Technology Center, 2790 Columbus Road, Bldg. 11-7, Granville, Ohio 43023-1200 (US).

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, LY, MA, MD, MG, MK, MN, MW, MX, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SM, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

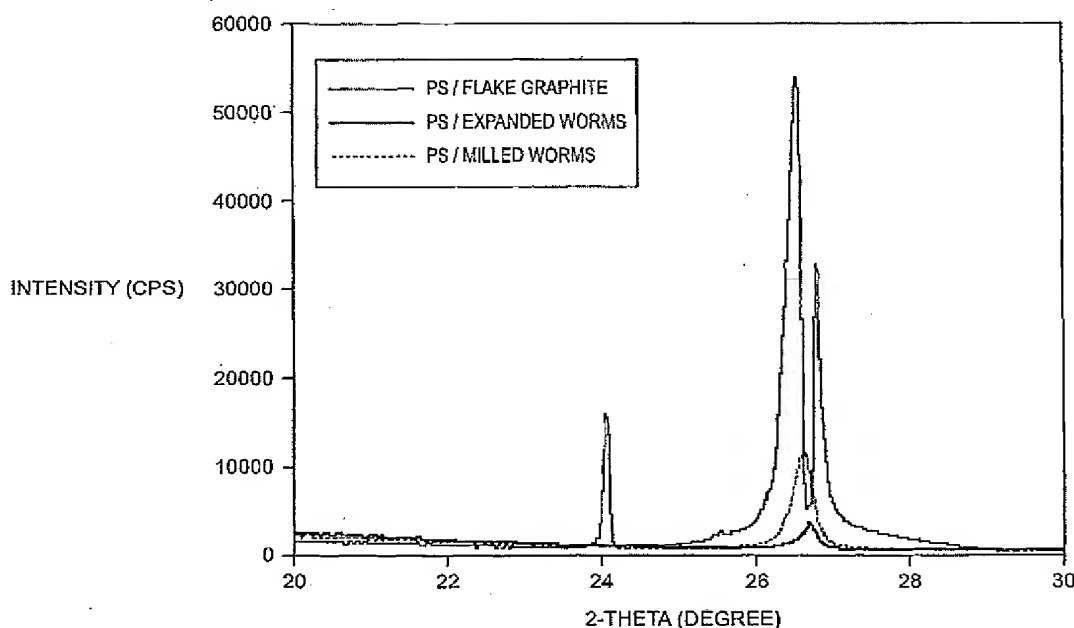
(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

- with international search report
- before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments

[Continued on next page]

(54) Title: POLYMER FOAMS CONTAINING MULTI-FUNCTIONAL LAYERED NANO-GRAPHITE



(57) Abstract: This invention relates to foam insulating products, particularly extruded polystyrene foam, containing multi-layered nano-graphite as a process additive for improving the physical properties of foam products.



For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

POLYMER FOAMS CONTAINING MULTI- FUNCTIONAL LAYERED NANO-GRAPHITE

TECHNICAL FIELD AND INDUSTRIAL

5 APPLICABILITY OF THE INVENTION

The present invention relates to rigid foamed polymeric boards containing multi-layered nano-graphite. More particularly, it relates to rigid foamed polymeric board wherein multi-layered nano-graphite is added as a process additive to improve the process, and to control the cell morphology, as well as to increase insulating capability, UV
10 stability, dimensional stability, and mechanical strength of the polymeric foamed board.

BACKGROUND OF THE INVENTION

The usefulness of rigid foamed polymeric boards in a variety of applications is well known. For instance, polymeric foam boards are widely used as insulating structural
15 members.

In the past, infrared attenuating agents (IAAs) such as carbon black powdered amorphous carbon, graphite, and titanium dioxide have been used as fillers in polymeric foam boards to minimize material thermal conductivity which, in turn, will maximize insulating capability (increase R-value) for a given thickness. Thermal conductivity, k is
20 defined as the ratio of the heat flow per unit cross-sectional to the temperature drop per unit thickness with the US unit:

$$\frac{\text{Btu} \cdot \text{in}}{\text{Hr} \cdot \text{Ft}^2 \cdot ^\circ\text{F}}$$

And the metric unit:

$$\frac{\text{W}}{\text{m} \cdot \text{k}}$$

The heat transfer through an insulating material can occur through solid conductivity, gas conductivity, radiation, and convection. The total thermal resistance (R-value), R is the measure of the resistance to heat transfer, and is determined as:

$$R = t / k$$

35 Where, t = thickness.

Rigid foamed plastic boards are extensively used as thermal insulating materials for many applications. It is highly desirable to improve the thermal conductivity without increasing the density, and /or the thickness of foam product. Particularly, the architectural community desires a foam board having a thermal resistance value of $R=10$, with a
5 thickness of less than 1.8 inches (4.57 cm), for cavity wall construction, to keep at least 1 inch (2.54 cm) of the cavity gap clean.

It is also desirable to improve the UV stability, particularly for such as exterior wall insulation finishing system (EIFS), and highway and railway underground applications where prolonged exposure of sun light of the surface of the polymer foam
10 boards are usually occurred in job-sites.

It is also desirable to improve the dimensional stability at elevated temperature and/or high humidity for such as indoor pool roofing, exterior wall insulation. U.S. 5,679,718 illustrates a microcellular extruded polystyrene foam containing graphite as an infrared attenuating agent (IAA). The IAA provide a greater proportional reduction in
15 foam thermal conductivity than foams having a larger cell size.

U.S. 6,420,442 shows a flame-proofed polystyrene foam material containing expanded graphite having a particle size of from 20 to 1000 micrometers. The foam is flame-retardant.

U.S. 6,213,540 illustrates an extruded thermoplastic foam having a high
20 compressive strength. The thermal resistance of the foam may be enhanced by adding fillers such as carbon black particulates, clay particulates or carbon or graphite fibers.

U.S. 3,574,644 shows a method of increasing the flame retardance of normally flammable materials by adding expandable graphite. Expanded graphite having a particle size of from about 10 to 325 mesh may be added to a film forming agent or other
25 polymeric materials such as polyesterds, polystyrene and polyethylene. Larger particles of graphite are preffed because the expansion ration of the larger flake is greater than that of a smaller flake.

U.S. 5,719,199 shows a flame retardant flexible, polymeric foam which contains expandable graphite as a fire retardant.

U.S. 5,854,295 illustrates a microcellular, polymeric foam containing an infrared attenuating (IAA) agent to reduce thermal conductivity. The IAA may be particulate flakes of metals or carbonaceous substances such as carbon black and natural or synthetic
30 graphite.

U.S. 6,387,968 shows a method for producing water expandable styrene polymers using water as a sole blowing agent. Styrene is polymerized in an aqueous suspension in the presence of from 0.1 to 15% by weight of a solid substance insoluble in water and in styrene such as carbon black or graphite. The graphite has an average particle size from
5 from 2 to 20 micrometers.

U.S. Patent Application Publication No. 2001/0036970 shows polymer foam having improved thermal insulating performance. The thermoplastic foam, typically made from polyethylene resin or polypropylene resin or blends thereof, may contain an IAA such as carbon black, graphite, or titanium dioxide to enhance thermal insulating capability.

10 U.S. Patent Application Publication No. 2003/0082343 illustrates a bendable thermoplastic foam which contains a slit to reinforce the foam. The foam may contain additives such as thermally insulating additives including aluminum, gold, silver, carbon black and graphite.

European Patent Application No. 729,000 shows a fire-retardant polymer
15 composition containing 100 parts by weight polyolefin or polystyrene, 1-30 parts by weight of an oxide or a complex oxide of metals such as antimony, boron and molybdenum and 1-30 parts of heat-expandable graphite. The graphite of a preferred particle size distribution contains the particles passing through a 80-mesh sieve at a content of 20% or lower by weight, more preferably from 1% to 20% by weight. Graphite containing the
20 particles at a content of lower than 1% by weight would slightly impair the shape-retaining properties of the resin composition when the resin composition is exposed to fire.

All of the above patents teach foams with 1 to 30 % by weight graphite -- either natural or synthetic graphite, or expandable graphite in the particle size around 2 to 1000 micrometers, having decreased thermal conductivity, and improved flame resistance.

25 Regular low density foams have very thin cell wall thickness in the range of 0.2 to 6 microns. Particularly, in order to enhance the insulation R-value, a target cell wall thickness of less than 0.1 micron is needed.

Thus, there is a need to graphite having at least in one dimension -- usually the thickness of the plate shaped graphite in nano-scale, that is, less than 0.1 microns or 100
30 nanometers. It is an object of the present invention to provide a process for preparing low density extruded polymer foams containing multi-layered nano-graphite which has good processing properties, and improved foam physical properties, including thermal

conductivity, ultraviolet (UV) radiation resistance, dimensional stability, mechanical strength, flame spread rate and smoke density.

The present invention relates to foam insulating products and the processes for making such products, such as extruded polystyrene foam, containing multi-layered nano-graphite as a process additive to improve the physical properties, such as thermal insulation and compressive strength. During foaming, multi-layered nano-graphite acts as a nucleator and lubricant as well as its slipping action makes the flow of the melted polymer in the extruder easier, and provides a smooth surface to the foam board. Further, the multi-layered nano-graphite reduces the amount of static present during the foaming process due to the increased electric conductivity of the skin of the nano-graphite polymer foam boards.

Multi-layered nano-graphite in a foam product also acts as a UV stabilizer and as a gas barrier in the final product.

It is an object of the present invention to produce a rigid polymer foam containing multi-layered nano-graphite which exhibits overall compound effects on foam properties including improved insulating value (increased R-value) for a given thickness and density, and ultraviolet (UV) stability.

It is another object of the present invention to produce a rigid polymer foam containing multi-layered nano-graphite having retained or improved compressive strength, thermal dimensional stability and fire resistance properties.

It is another object of the present invention to provide multi-layered nano-graphite in a rigid polymer foam which also acts as a process additive which control the cell morphology, reduces static and provides lubrication during the foaming process.

It is another object of the present invention to lower the cost of a polymeric foam product in a simple and economical manner, such as by using multi-layered nano-graphite as a low cost, functional colorant.

The foregoing and other advantages of the invention will become apparent from the following disclosure in which one or more preferred embodiments of the invention are described in detail and illustrated in the accompanying drawings. It is contemplated that variations in procedures, structural features and arrangement of parts may appear to a person skilled in the art without departing from the scope of or sacrificing any of the advantages of the invention.

BRIEF DESCRIPTION OF DRAWINGS

Fig. 1 is a graphical illustration showing the x-ray diffraction pattern of various forms of graphite in polystyrene polymer foam.

Fig. 2 is a diagram of a treatment used on the graphite of the present invention.

5 Figs. 3a – 3d are optical microscope images of multi-layered nano-graphite dispersed in polystyrene.

Figs 4a – 4d are SEM images of polystyrene foam cell walls and struts containing multi-layered nano-graphite.

10 Fig. 5 is a graphical illustration showing a comparison of polystyrene foam containing talc vs. polystyrene foam containing multi-layered nano-graphite.

Fig. 6 is a TEM (transmission electron microscope) image showing the 3% milled, expanded, multi-layered nano-graphite distribution in polystyrene foam.

DETAILED DESCRIPTION OF INVENTION

15 The above objects have been achieved through the development of a rigid, polymer foam which contains multi-layered nano-graphite to provide infrared attenuation, controls cell morphology and acts as a gas diffusion barrier. The foam exhibits improved thermal insulation (R-values). The present invention particularly relates to the production of a rigid, closed cell, polymer foam board prepared by extruding process with multi-layered
20 nano-graphite, at least one blowing agent and other additives.

The rigid foamed plastic materials may be any such materials suitable to make polymer foams, which include polyolefins, polyvinylchloride, polycarbonates, polyetherimides, polyamides, polyesters, polyvinylidene chloride, polymethylmethacrylate, polyurethanes, polyurea, phenol-formaldehyde,
25 polyisocyanurates, phenolics, copolymers and terpolymers of the foregoing, thermoplastic polymer blends, rubber modified polymers, and the like. Suitable polyolefins include polyethylene and polypropylene, and ethylene copolymers.

A preferred thermoplastic polymer comprises an alkenyl aromatic polymer material. Suitable alkenyl aromatic polymer materials include alkenyl aromatic
30 homopolymers and copolymers of alkenyl aromatic compounds and copolymerizable ethylenically unsaturated comonomers. The alkenyl aromatic polymer material may further include minor proportions of non-alkenyl aromatic polymers. The alkenyl aromatic polymer material may be comprised solely of one or more alkenyl aromatic

homopolymers, one or more alkenyl aromatic copolymers, a blend of one or more of each of alkenyl aromatic homopolymers and copolymers, or blends of any of the foregoing with a non-alkenyl aromatic polymer.

Suitable alkenyl aromatic polymers include those derived from alkenyl aromatic compounds such as styrene, alphas-methylstyrene, ethylstyrene, vinyl benzene, vinyl toluene, chlorostyrene, and bromostyrene. A preferred alkenyl aromatic polymer is polystyrene. Minor amounts of monoethylenically unsaturated compounds such as C₂₋₆ alkyl acids and esters, ionomeric derivatives, and C₄₋₆ dienes may be copolymerized with alkenyl aromatic compounds. Examples of copolymerizable compounds include acrylic acid, methacrylic acid, ethacrylic acid, maleic acid, itaconic acid, acrylonitrile, maleic anhydride, methyl acrylate, ethyl acrylate, isobutyl acrylate, n-butyl acrylate, methyl methacrylate, vinyl acetate and butadiene

Preferred structures comprise substantially (that is, greater than about 95 percent) and most preferably entirely of polystyrene. The present invention relates to a process for preparing a foam product involving the steps of forming a foamable mixture of (1) polymers having weight -average molecular weights from about 30,000 to about 500,000. In one embodiment, the polystyrene has weight-average molecular weight about 250,000, and (2) multi-layered nano-graphite, (3) a blowing agent, (4) other process additives, such as a nucleation agent, flame retardant chemicals, foaming the mixture in a region of atmosphere or reduced pressure to form the foam product.

The nano-graphite used in this invention is a multi-layered nano-graphite which has at least in one dimension, most likely the thickness of the particle, less than about 100 nanometers.

The multi-layered nano-graphite of the present invention may be in one of the following forms: an intercalated, or exfoliated, multi-layered nano-graphite such as by furnace high temperature expansion from acid-treated natural graphite, or microwave heating expansion from moisture saturated natural graphite.

It is preferable that the above expanded graphite be mechanically treated such as by air jet milling to pulverize the nano-graphite particles. The pulverization of the particles ensures that the nano-graphite flake thickness is less than 100 nm, and that the other dimensions of particles are less than about 20 microns, most likely less than about 5 microns.

It is preferable that the above expanded graphite be chemically treated, that is, grafting, so as to induce carboxyl and phenolic hydroxyl functional groups on the graphite edge, that is, or further grafting with other functional group. Grafting of the graphite enables the graphite to be more dispersive in the polymer foam.

5 Standard graphing procedures may be utilized; however an example of one treatment is oxidation where the surface of the graphite is oxidized. Acid is added to the nano-graphite causing a strong oxidation reaction between concentrated nitric acid and carbons on graphite surfaces so as to induce carboxyl and phenolic hydroxyl functional groups on the graphite surface. In this method the graphite is boiled in 70% nitric acid at a
10 temperature between 115°C and 140°C. Another method which may be used to oxidize the graphite surface involves exposing the graphite to an oxidic gas or a mixture of reactive gases.

It is preferable that the chemically treated expanded graphite be further grafted with other functional groups, for example acid treated graphite containing carboxylic acid
15 groups on the carbon surface further functionalized with glycidyl methacrylate (GMA) to improve the dispersion of the resulting graphite in polymers.

After treatment of the graphite, the polymer and multi-layered nano-graphite and prepared via in-situ polymerization. It is preferably to use a monomer, such as styrene, methyl methacrylate, or a mixture of monomers. Preferably, styrene monomer and an
20 initiator (catalyst), such as benzoyl peroxide (BPO), or 2,2' - azobisisobutyronitrile (AIBN), are blended together completely using a conventional mixing apparatus such as a homogenizer. The multi-layered nano-graphite is then added to the styrene-initiator mixture in an amount of preferably about 0.1 to about 10%, more preferably about 0.5 to about 5% by weight based on the weight of the polymer. After mixing, the mixture is
25 heated in an oven at a temperature of about 60°C to 100°C, for about 15 to 30 hours for in-situ polymerization.

In mixing the graphite with the polystyrene monomer, as discussed above, it is important to have uniform distribution of the graphite. As such, the surface of the acid treated graphite, as mentioned above, may be functionalized with glycidyl methacrylate
30 (GMA). An example of the surface treatment of the graphite using GMA follows in Example 1 which is not to be construed as limiting.

The multi-layered nano-graphite may also be melted and blended with polymer carriers, such as polystyrene, polymethyl methacrylate (PMMA), ethyl methacrylate

(EMA). The loading can be as high as 40%. Mixing temperature is about 150°C to about 300°C, typically about 225°C for EMA, and mixing time about 0 to about 3 minutes; typically less than one minute for EMA carrier containing 40 percent by weight nano-graphite, are crucial for effective dispersing of nano-graphite throughout the polymer.

5 Mixing may be conducted by any standard method known in the art. Preferably, the components are mixed using a Banbury mixer.

After in-situ polymerization or melt compounding, the multi-layered nano-graphite/polystyrene compound is foamed using a batch foaming process or standard extrusion process. Extruded polystyrene is made by continuously extruding molten
10 polystyrene containing a blowing agent under elevated temperature and pressure into ambient or vacuum conditions, allowing the mass to expand into a lightweight, closed-cell foam.

Standard extrusion processes and methods which may be used in the process of manufacturing the invention are described in commonly owned U.S. Patent 5,753,161.

15 In the extrusion process, an extruded polystyrene polymer, multi-layered, nano-graphite foam is prepared by twin-screw extruders (low shear) with flat die and plate shaper. Alternatively, a single screw tandem extruder (high shear) with radial die and slinky shaper can be used. Multi-layered nano-graphite is then added into the extruder preferably about 0.1 to about 10%, more preferably about 0.5 to about 3% by weight based
20 on the weight of the polymer along with polystyrene, a blowing agent, and optionally other additives. In a preferred embodiment, an extruded polystyrene polymer foam is prepared by twin-screw extruders (low shear) with flat die and plate shaper. Alternatively, a single screw tandem extruder (high shear) with radial die and slinky shaper can be used. Preferably, the multi-layered nano-graphite compound is added into the extruder via multi-
25 feeders, along with polystyrene, a blowing agent, and/or other additives.

The plastified resin mixture, containing multi-layered nano-graphite, polymer, and optionally, other additives are heated to the melt mixing temperature and thoroughly mixed. The melt mixing temperature must be sufficient to plastify or melt the polymer. Therefore, the melt mixing temperature is at or above the glass transition temperature or
30 melting point of the polymer. Preferably, in the preferred embodiment, the melt mix temperature is from about 200°C to about 250°C, most preferably about 220°C to about 240°C depending on the amount of multi-layered nano-graphite.

A blowing agent is then incorporated to form a foamable gel. The foamable gel is then cooled to a die melt temperature. The die melt temperature is typically cooler than the melt mix temperature, in the preferred embodiment, from about 100°C to about 130°C, and most preferably from about 120°C. The die pressure must be sufficient to prevent prefoaming of the foamable gel, which contains the blowing agent. Prefoaming involves the undesirable premature foaming of the foamable gel before extrusion into a region of reduced pressure. Accordingly, the die pressure varies depending upon the identity and amount of blowing agent in the foamable gel. Preferably, in the preferred embodiment, the pressure is from about 50 to about 80 bars, most preferably about 60 bars. The expansion ratio, foam thickness per die gap, is in the range of about 20 to about 70, typically about 60.

Any suitable blowing agent may be used in the practice on this invention. Blowing agents useful in the practice of this invention include inorganic agents, organic blowing agents and chemical blowing agents. Suitable inorganic blowing agents include carbon dioxide, nitrogen, argon, water, air, nitrogen, and helium. Organic blowing agents include aliphatic hydrocarbons having 1-9 carbon atoms, aliphatic alcohols having 1-3 carbon atoms, and fully and partially halogenated aliphatic hydrocarbons having 1-4 carbon atoms. Aliphatic hydrocarbons include methane, ethane, propane, n-butane, isobutane, n-pentane, isopentane, and neopentane. Aliphatic alcohols include methanol, ethanol, n-propanol, and isopropanol. Fully and partially halogenated aliphatic hydrocarbons include fluorocarbons, chlorocarbons, chlorofluorocarbons and cyclopentane. Examples of fluorocarbons include methyl fluoride, perfluoromethane, ethyl fluoride (HFC-161), ethyl fluoride, 1,1-difluoroethane (HFC-152a), 1,1,1-trifluoroethane (HFC-143a), 1,1,1,2-tetrafluoro-ethane (HFC-134a), 1,1,2,2-tetrafluoroethane (HFC-134), pentafluoroethane (HFC-125), difluoromethane (HFC-32), perfluoroethane, 2,2-difluoropropane (HFC-272fb), 1,1,1-trifluoropropane (HFC-263fb), perfluoropropane, 1,1,1,3,3-pentafluorobutane (HFC-365mfc), 1,1,1,3,3 – pentafluoropropane (HFC 245fa), 1,1,1,2,3,3,3-heptafluoropropane (HFC-227ea), dichloropropane, difluoropropane, perfluorobutane, and perfluorocyclobutane. Partially halogenated chlorocarbons and chlorofluorocarbons for use in this invention include methyl chloride, methylene chloride, ethyl chloride, 1,1,1-trichloroethane, 1,1-dichloro-1-fluoroethane (HCFC-141b), 1-chloro-1,1-difluoroethane (HCFC-142b), chlorodifluoromethane (HCFC-22), 1,1-dichloro-2,2,2-trifluoroethane (HCFC-123) and 1-chloro-1,2,2,2-tetrafluoroethane (HCFC-124), and the

like. Fully halogenated chlorofluorocarbons include trichloromonofluoromethane (CFC-11), dichlorodifluoromethane (CFC-12), trichlorotrifluoroethane (CFC-113), 1,1,1-trifluoroethane, pentafluoroethane, dichlorotetrafluoroethane (CFC-114), chloroheptafluoropropane, and dichlorohexafluoropropane. Chemical blowing agents
5 include azodicarbonamide, azodiisobutyro-nitrile, benzenesulfonhydrazide, 4,4-oxybenzene sulfonyl-semicarbazide, p-toluene sulfonyl semi-carbazide, barium azodicarboxylate, and N,N'-dimethyl-N,N'-dinitrosoterephthalamide and trihydrazino triazine.

In the present invention it is preferable to use about 6 to about 14%, preferably
10 about 11%, cyclopentane by weight based on the weight of the polymer. It is preferred to add about 0 to about 4% ethanol, about 3 to about 6%, preferably about 3.5% carbon dioxide. All percentages are based on the weight of the polymer.

Optional additives may be incorporated in the extruded foam product and include additional infrared attenuating agents, plasticizers, flame retardant chemicals, pigments,
15 elastomers, extrusion aids, antioxidants, fillers, antistatic agents, UV absorbers, citric acids, nucleating agents, surfactants, processing aids. These optional additives may be included in any amount to obtain desired characteristics of the foamable gel or resultant extruded foam products. Preferably, optional additives are added to the resin mixture but may be added in alternative ways to the extruded foam manufacture process.

The product produced by the above-described process is a rigid, foam insulation
20 board which is about 1/8 to 12 inches (0.32 to 30.48 cm) thick, typically 1 to 4 inches (2.54 to 10.16 cm) thick. The density of the foam board is typically about 1.2 to about 5 pcf (19.22 to 80.09 kg/m³), typically about 1.4 to about 3 pcf (22.43 to 48.06 kg/m³).

Having generally described this invention, a further understanding can be obtained
25 by reference to certain specific examples illustrated below which are provided for purposes of illustration only and are not intended to be all inclusive or limiting unless otherwise specified.

Example 1

30 Functionalization of Graphite

One gram of graphite was homogenized in 200 ml dimethyl formamide (DMF) solvent for three minutes and then sonicated for 30 minutes to form a dark suspension. GMA (0.464 g) was dissolved in 100 ml DMF separately and then mixed with the

previous graphite suspension. Upon adding concentrated sulfuric acid as the catalyst, the reaction mixture was magnetically stirred at 65°C for 24 hours. The suspension was then cooled down and filtered to form a wet cake. The cake was washed with additional DMF until the filtrate was clear. The wet cake was dried under vacuum at 70°C overnight to
5 remove the residual solvent. The fluffy resulting material (0.81g) was GMA-functionalized graphite. Fig. 2 illustrates a comparison of the structure of the acid-treated graphite and the GMA-graphite.

The dispersion of both acid-treated graphite and GMA-functionalized graphite in the styrene monomer was investigated using optical microscopy as shown in Fig. 3. Four
10 different suspensions (a-d) were prepared in this study showing 1% graphite by weight of the styrene monomer. In (a), acid-treated graphite without homogenization or ultra-sonication is shown. Fig. 3(b) shows acid-treated graphite, with homogenization (3 mins.) and ultra-sonication (30 mins.). Comparing (a) and (b), it shows that when using certain mechanical forces, such as homogenization and ultra-sonication, a better dispersion of
15 graphite was achieved. However, there are still considerably large amounts of agglomerates existing in suspension (b). Suspension (c) was GMA-functionalized graphite dispersed in the styrene without homogenization or ultra-sonication. As shown in (c), even without further shear-mixing or sonication, the dispersion of graphite was substantially improved as compared to that in (b). Furthermore, if suspension (c) was also
20 homogenized and sonicated for a certain while, a uniform distribution of finer graphite particles could be obtained, as shown in (d) which shows GMA-functionalized graphite with homogenization (3 minutes) and ultra-sonication (30 minutes). Using this chemical treatment, the dispersion of the resulting graphite is substantially improved.

25

Example 2

The invention is further illustrated by the following Example 2, which is not to be construed as limiting, in which all foam boards are extruded polystyrene foam boards. In the following samples and control samples, rigid polystyrene foam boards are prepared by a twin screw LMP extruder with flat die and shaper plate; and a two single screw tandem
30 extruder with radial die and slinky shaper. A vacuum may also be applied in both of the above described pilot and manufacturing lines.

Table 1 shows the process conditions for samples in a twin screw extruder for making foam boards having a width of 16 inches (40.64 cm) and a thickness of 1 inch (2.54 cm).

Table 1 - Process Conditions of Samples

	Samples on Table 6
Wt. % of nano-graphite	1 to 5
Wt. % of talc	0.5 - 1.5
Wt. % of nano-carbon black	0 to 6
Wt. % of mica	0 to 4
Wt. % of HCFC-142b	11
Wt. % of CO ₂	0
Extruder Pressure, Kpa (psi)	13000 - 17000 (1950 - 2400)
Die Melt Temperature, (°C)	117 - 123
Die Pressure, Kpa (psi)	5400 - 6600 (790 - 950)
Line Speed, m/hr (ft/min)	110 - 170 (6 - 9.5)
Throughput, kg/hr	100
Die Gap, mm	0.6 - 0.8
Vacuum KPa (inch Hg)	0 - 3.4 (0 to 16)

Nano-graphite used was prepared from expanded graphite, as discussed above, which was further treated by melt compounding with polystyrene. The graphite loading and carrier are specified in Table 2 (compounds A and B). Stabilized hexabromocyclododecane (Great Lakes Chemical, HBCD SP-75) was used as flame retardant agent in the amount of 1% by weight of the solid foam polymer.

Table 2 - Materials for Compound A & B

	Graphite Type	Exfoliated Graphite (Description)	Carrier
A	Nano Grafoil MB	Fine size expanded graphite, less than 10 um from GraphTech, 40% loading	Ethyl methacrylate (EMA)
B	Graphite Nano-Concentrate	Grade LBG expanded graphite from Superior Graphite, 40% loading	Polystyrene (Melt Index 8)

The results of above examples are shown in Table 3. All R-values and compressive strength are tested after the samples aged for more than 30 days, unless otherwise indicated.

Table 3 - Melt Blending Layered Graphite/PS Foam

Run #	Aged R-value K.m2/K (F.ft2.hr/ Btu)	Density Kg/m3 (pcf)	Average Cell micron	Compressive Strength psi	Nano-graphite Wt%
Control sample	0.792 (5.49)	27.68 (1.73)	240	NA	0
696-2	0.907 (6.29*)	28.64 (1.79)	220	21.55	1 (compound A)
696-4	0.949 (6.58*)	30.72 (1.92)	174	22.67	3 (compound A)
692-2	0.891 (6.18)	27.84 (1.74)	222	25.69	1 (compound B)
692-3	0.916 (6.35)	28.8 (1.80)	187	27.27	2 (compound B)
692-4	0.92 (6.38)	28.96 (1.81)	169	26.87	3 (compound B)

*When aged 180 days, sample 696-2 R=5.8; and sample 696-4, R=6.1

As shown from above samples, the addition of nano-graphite in foaming processing, preferably about 0.25 to about 3 % by the weight of the solid foam polymer has profound effect on the thermal resistance property, an enhancement of R-value from about 8% to about 20% of the foam board products. The in-situ polymerized, exfoliated nano-graphite with surface chemical modification was the most effective, intercalated expanded nano-graphite by melt-blending is also effective with a much lower cost.

Example 3

Table 4 compares the operating conditions between batch foaming and traditional low-density foam extrusion.

Table 4 - Comparison of Operating Conditions between Batch and Extrusion Foaming

Operating conditions	Extrusion	Batch Foaming
Temperature (°C)	100 ~ 140	120
Pressure (psi)	1000 ~ 2000	2000
dP/dt (Pa/sec)	10 ⁶	10 ⁶

Prior to batch foaming, the polymerized multi-layered nano-graphite/polystyrene compound is heated and compressed into a solid shape. The solid sheet is cut into small pieces according to the size of pressure vessel, such as 77 x 32 x 1 mm. The solid sheet

specimen is then placed in a mold and foamed in a high-pressure vessel at about 80°C to about 160°C, typically about 120°C and about 500 to about 4000 psi, typically about 2000 psi. The solid sheet remains in the pressurized vessel for about 8 to about 50 hours, typically about 12 hours, after which the pressure in the vessel was released quickly (about 12 seconds) for foaming.

The multi-layered nano-graphite/polystyrene foam of the batch foaming samples were evaluated to determine the amount infrared radiation transmitted through the foam. As infrared light is the major form of thermal radiation.

A piece of batch-foamed sample containing polystyrene and about 3% graphite, and two other comparison samples containing polystyrene or polystyrene and 5% nano-clay were selected. On one side of the foam sample a light source of infrared laser was placed. On the other side of the sample, either a detector was placed to record the transmission light intensity or a temperature camera was placed to monitor the surface temperature change. The results are summarized in Tables 5 and below.

Table 5 - Infrared Light Transmission
Through foam samples of polystyrene (PS), polystyrene and 5% nano-clay (PS/5% clay), and polystyrene and 3% nano-graphite (PS/3% graphite)

IR Transmission Intensity (watts)	Emissive Intensity	Received Intensity	%Trans
PS (control sample)	0.5	0.05	10%
PS/5% MHABS*	0.5	0.02	4%
PS/3% milled graphite worms	0.5	0.01	2%

*in-situ polymerized compound with 5% of reactive cationic surfactant, 2-methacryloyloxyethylhexadecyldimethyl ammonium bromide (MHAB) treated Na⁺ montmorillonite with 95% styrene monomer

As shown in Table 5, 10% of the light transmits through the pure PS foam sample, while only 4% through the PS/5% clay foam sample and only 2% through the PS/3% graphite sample. Both clay and graphite have the attenuation effect on the infrared light, however, as shown in the above table, PS/3% graphite has considerably better transmission attenuation.

The temperature of the PS/graphite sample, on the side of the sample opposite to the light source, was slightly elevated, having an increase of about 2°F - 3°F after 60 seconds of exposure (Table 6). There was no obvious change in surface temperature for foam samples of pure PS and PS/clay. As such, PS/graphite foam attenuates thermal

radiation and enhances the heat solid conduction. Further, by improved graphite dispersion and concentration, these trends are expected to be more significant.

Table 6 - Temperature change for foam samples of PS, PS/5% clay, and PS/3% graphite on the surface opposite to the light source

	IR Camera Temperature at Interval Time in Seconds						
	°F						
	0	10	20	30	40	50	60
PS (control sample)	78.4 °F	78.4 °F	78.7 °F	78.8 °F	78.4 °F	78.5 °F	78.5 °F
PS/5% MHABS	79.2 °F	79.2 °F	79.5 °F	79.6 °F	79.4 °F	79.5 °F	79.6 °F
PS/3% milled graphite worms	80.6 °F	81.2 °F	81.7 °F	82 °F	82.6 °F	82.8 °F	83 °F

Example 4

By using a foaming extrusion die, foam samples having different compositions with similar densities were prepared (Fig. 4 a – d). The corresponding cell morphology and the important thermal and mechanical properties, including compressive properties, IR radiation transmission, and flammability, were analyzed.

Atofina (CX 5197) polystyrene was used as received (pellet form). All samples described in this study contain 1 wt% HBCD-SP flame retardant from Great Lakes. The polystyrene/multi-layered nano-graphite compound was mechanically blended at 185°C using a twin-screw extruder (Leistritz ZSE-27; L/D = 40; D = 27mm).

Foam extrusion for each material is carried out by pumping the blowing agent into the twin-screw extruder using a syringe pump. Atofina supplied the HCFC blend for this study; (H142B/22) 60% by weight HCFC-142b, and 40% by weight R-22. During the experiments, H142B/22 was used as the foaming agent and its content was 11 wt% by weight of polymer. The foaming temperature in the die was 35°C and the die pressure was around 850 psi. The mass flow rate of the polymer melt was around 90 grams/min.

All properties were tested on rectangular samples with 4 to 6 mm in thickness and 80 to 100 mm in width. The specimens are prepared by cutting segments out of extruded foams, and test results of aged insulation R-value of example 2 as shown on Table 7.

Table 7 - In-situ Nano-Graphite/PS Foam

Run #	Aged R-value K.m ² /K (F.ft ² .hr/Btu)	Amount of Layered Graphite Wt%	Amount of Talc Wt%	Average Cell micron	Blowing Agent Wt%
Control Sample	0.766 (5.31)	0	1	155	HCFC 142b 6%; R-22 4%
040122 -03	0.826 (5.73)	0.25	0	100	HCFC 142b 6%; R-22 4%

Figure 4 illustrates the foam structure for the samples after adding multi-layered nano-graphite. Compared with the polystyrene (PS)/1 wt% talc foam sample (Fig. 4a), the addition of graphite significantly decreases the foam cell size and increases the cell density, indicating the graphite is an effective nucleating agent of polystyrene with H142B/22 as the foaming agent. When the concentration of the milled graphite worms increases from 0.25 wt% (Fig. 4 b) to 0.5 wt% (Fig. 4c), the cell density is further increased. Fig. 5 further illustrates the trend. After adding 0.25% milled graphite worms in polystyrene, the cell size decreases to 81 μm from 155 μm of the polystyrene/1 wt% talc foam sample and the cell density increases to 1.6×10^6 cells/cc from 2.3×10^5 cells/cc.

As shown, the addition of multi-layered nano-graphite shrinks the cell wall thickness and the strut size, which may influence the mechanical strength and the insulation property. When 0.25 wt% milled nano-graphite worms are present in polystyrene foam, the R-value increases 8% from 5.31 K.m²/K of polystyrene/1 wt% talc foam sample to 5.73 K.m²/K. Furthermore, by exposing the graphite samples under intensive UV light, it shows no significant change after 1000 hours; however, the sample without graphite has already cracked after the same treatment. The graphite foam sample provides excellent properties in insulation and UV resistance.

Figure 6 is a TEM image of multi-layered nano-graphite in a polystyrene matrix.

Example 5

The following table shows a comparison of the oxygen content between chemically-treated graphite and untreated graphite.

Table 8 – Oxygen Content of Polystyrene Foams Containing

Treatment	Oxygen Content %
Chemically-modified expanded graphite with HNO ₃ at 115°C -140°C	2.8
Chemically-modified expanded graphite with reactive gas	2.2
Untreated expanded graphite	2

Example 6

Fig. 1, shows an X-ray diffraction graph confirming that there is no significant change in d-value of 002 peaks ($2\theta = 26.4 \sim 26.7^\circ$), which is around 3.33 ~ 3.35 angstroms, a typical d-spacing between carbon layers in graphite. This indicates that the expansion does not happen in each individual gallery spaces of graphite carbon layers. Expanded graphite, or so called worms or “exfoliation” of graphite in which graphite expands by hundreds of times along the c-axis (002 direction), is usually obtained by rapid heating of a graphite intercalation compound (GIC). The most common choice of intercalation compound is graphite bisulphate obtained by reaction with a mixture of sulphuric and nitric acids because of its ability to yield expansions as high as several hundreds time. The expanded graphite particle is composed of many nanosheets having a thickness of about 10 to about 100 nm. Each nanosheet is made up of many single carbon layers of graphite with the d-space having no significant change as shown in Fig. 1 after macro-scale exfoliation.

Table 9 shows examples of the total layer thickness of the expanded nano-graphite worms (without polystyrene) and milled nano-graphite worms (without polystyrene) compared to (PS)/nano-graphite samples after different treatments by X-ray diffraction (XRD) characterization. The following is an explanation of the XRD process.

When determining lattice parameters of exfoliated expanded graphite, the graphite layer structure keeps the same, for a particular d involved, for example 002, the Bragg angle θ to satisfy will not be change according to Bragg law:

$$\lambda = 2 d \sin \theta$$

This indicates that there is no change in the d-space for each individual crystal. However, after expanding, the thickness of graphite crystals decreases. Therefore, the width of the diffraction curve increases as the thickness of the crystals decreases according to Scherrer formula:

$$t = 0.9 \lambda / B \cos \theta$$

Where,

λ , the wave length, for the Cu K α_1 line, 1.540562 Å

d is the lattice space, for the graphite 002, around 3.37 Å

5 θ is diffraction angle, the 002 peak for graphite 2θ around 26.45 °

t is the thickness of the m layered graphite, $t = md$

B is the angular width at an intensity equal to half the maximum intensity, a rough measurement:

$$B = \frac{1}{2} (2\theta_1 - 2\theta_2)$$

10 Where, the two limiting angles, $2\theta_1$ and $2\theta_2$, at which the diffracted intensity drops to zero.

It was observed that the expanded graphite and its composite with polystyrene, the full width, B at half maximum became broader as shown in the following table and figures. The calculated thickness, t of layered graphite is about 50 nm.

15 There is no change of the d -spacing between the lattice planes (002). This indicates that there is no exfoliation, nor exfoliation between the multi-layered graphite. However, it is important to note that the multi-layered nano-graphite and its composite with polystyrene, the full width, B at half maximum, became broader as shown in the following Table 9 and in figure 1. The calculated thickness, t , of layered nano-graphite is less than
20 about 100 nm, typically about 50 nm.

Table 9
X-ray diffraction of graphite and polystyrene (PS/graphite composites)

	2θ (°)	d (Å)	Miller Indices hkl	B (°)	Crystal Thickness t (nm)
Samples	26.45	3.37	002	0.190	43.0
Expanded worms*	26.72	3.33	002	0.095	86.0
Milled worms	26.56	3.35	002	0.275	29.7
PS/Flake graphite	26.54	3.36	002	0.125	65.3
PS/Expanded worms	26.69	3.33	002	0.160	51.0
PS/Milled worms	26.65	3.34	002	0.170	48.0

* the profile of the peak is not perfect for B -value calculation

The foregoing description of the specific embodiments will so fully reveal the general nature of the invention that others can, by applying knowledge within the skill of the art (including the contents of the references cited herein), readily modify and/or adapt

for various applications such specific embodiments, without undue experimentation, without departing from the general concept of the present invention. Therefore, such adaptations and modifications are intended to be within the meaning and range of equivalents of the disclosed embodiments, based on the teaching and guidance presented herein. It is to be understood that the phraseology or terminology herein is for the purpose of description and not of limitation, such that the terminology or phraseology of the present specification is to be interpreted by the skilled artisan in light of the teachings and guidance presented herein, in combination with the knowledge of one of ordinary skill in the art.

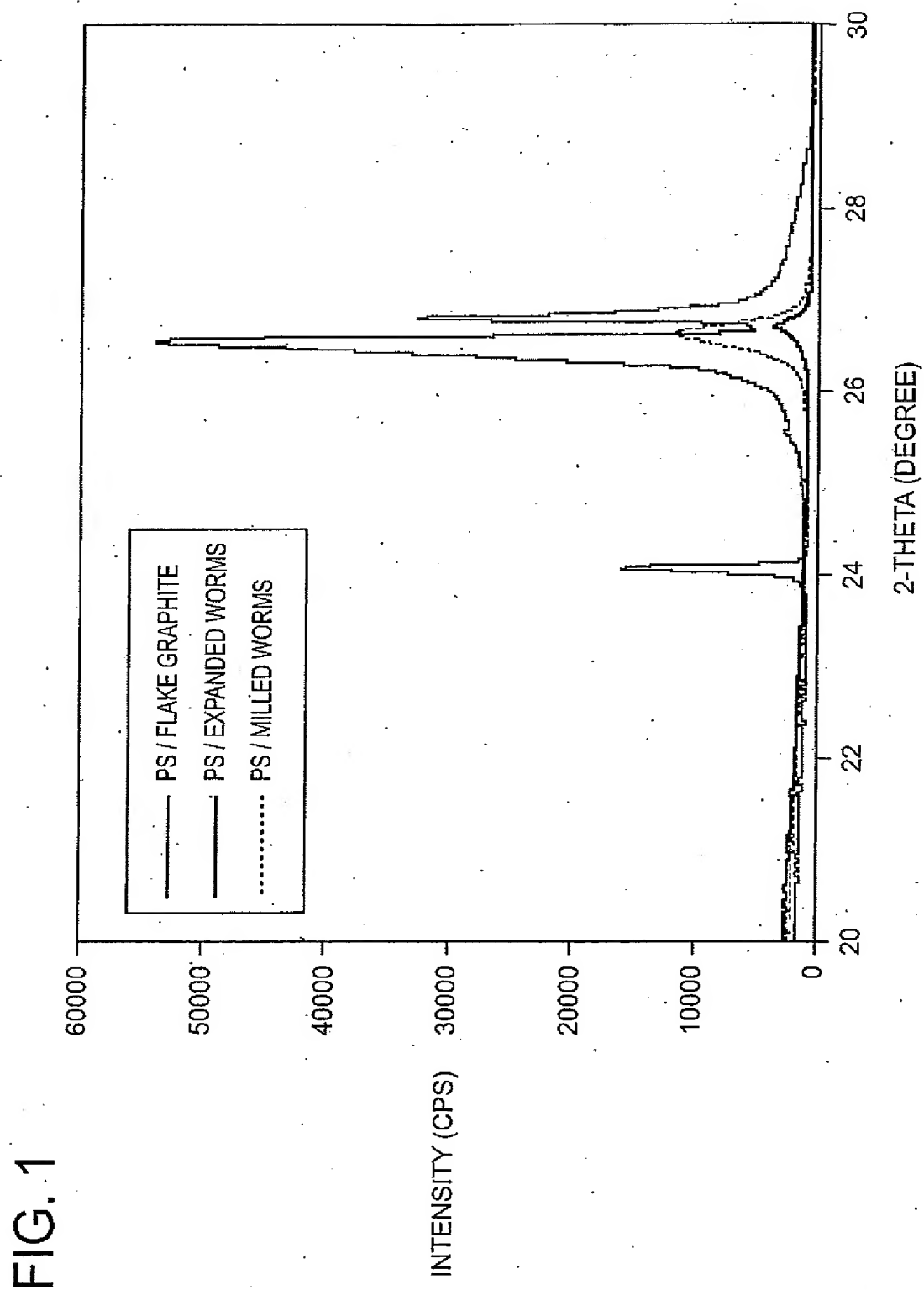
The invention of this application has been described above both generically and with regard to specific embodiments. Although the invention has been set forth in what is believed to be the preferred embodiments, a wide variety of alternatives known to those of skill in the art can be selected within the generic disclosure. The invention is not otherwise limited, except for the recitation of the claims set forth below.

WHAT IS CLAIMED IS:

1. A multi-functional polymeric foam material comprising:
 - a) a polymer;
 - b) a blowing agent; and
 - c) multi-layered nano-graphite.
2. The multi-functional polymeric foam material of claim 1, wherein the multi-layered nano-graphite is present in an amount of from about 0.1 to about 10% by weight based on the polymer.
3. The multi-functional polymeric foam material of claim 2, wherein the multi-layered nano-graphite is presented in an amount of from about 0.5% to about 3% by weight based on the polymer.
4. The multi-functional polymeric foam material of claim 1, further comprising one or more additives selected from the group consisting of cell size enlarge agents, infrared attenuating agents, plasticizers, flame retardant chemicals; pigments, elastomers, extrusion aids, antioxidants fillers, antistatic agents and UV absorbers.
5. The multi-functional polymeric foam material of claim 1, wherein said multi-layered nano-graphite further comprises a plurality of nanosheets.
6. The multi-functional polymeric foam material of claim 5, wherein said plurality of nanosheets have a thickness of between about 10 to several hundred nanometers, with majority in the range from about 10 to about 100 nanometers.
7. The multi-functional polymeric foam material of claim 6, wherein said plurality of nanosheets comprises a plurality of single carbon layers of graphite.
8. The multi-functional polymeric foam material of claim 10, wherein the surface of said plurality of nano-sheets is grafted with carboxyl and hydroxyl groups.
9. The multi-functional polymeric foam material of claim 1, wherein the R-value of said material is between about 3 to about 8.
10. The multi-functional polymeric foam material of claim 1, wherein the percent of infrared light transmission is between about 0 to about 2%.
11. A method for making a multi-functional extruded polymer foam comprising the steps of:
 - a) mixing a resin mixture comprising a polymer and multi-layered nano-graphite compound;
 - b) heating said resin mixture to a melt mixing temperature;

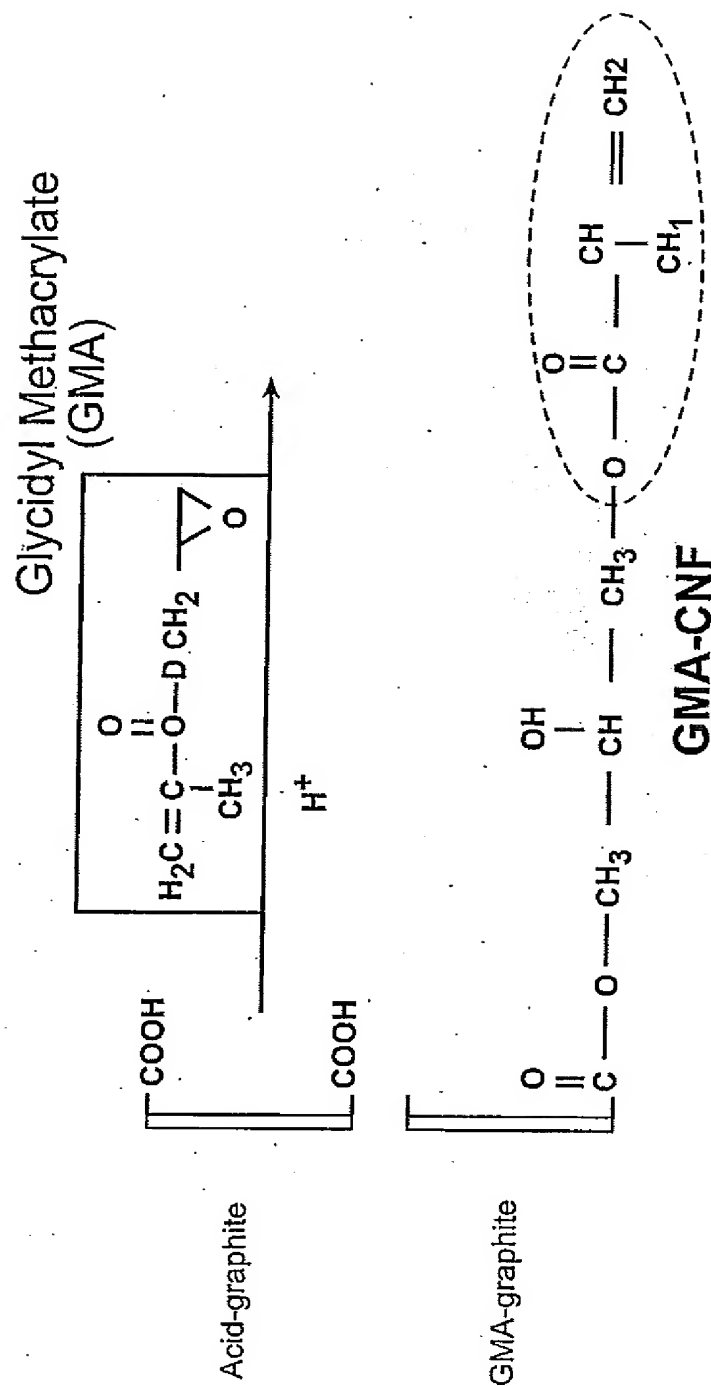
- c) incorporating one or more blowing agents into the resin mixture under a pressure sufficient to prevent pre-foaming of the gel;
 - d) cooling the gel to a die melt temperature; and
 - e) extruding the gel through a die to a region of lower die pressure to form the foam.
12. The method of claim 11, wherein the nano-graphite compound is added in an amount of from about 2 to about 100 % by weight based on the polymer.
13. The method of claim 12, wherein the nano-graphite is added in an amount of from about 0.5% to 10% by weight based on the polymer.
14. The method of claim 11, further comprising the step of mixing one or more additives selected from the group consisting of cell size enlarge agents, infrared attenuating agents, plasticizers, flame retardant chemicals, pigments, elastomers, extrusion aids, antioxidants fillers, antistatic agents and UV absorbers into the mixture
15. The method of claim 11, wherein the polymer is polystyrene.
16. A method for making a batch polymer foam comprising the steps of:
- a) adding extruded or molded polymer solid containing nano-graphite to a pressure vessel;
 - b) adding at least one blowing agent to the pressure vessel;
 - c) pressurizing said pressure vessel to a level sufficient to force an appropriate amount of the blowing agent into the free volume of the polymer.
 - d) reducing the pressure and removing said roll of polymer containing nano-graphite from the pressure vessel when the blowing agent has thoroughly saturated the polymer.
17. A rigid foam insulation board comprising:
- a) a polymer;
 - b) a blowing agent; and
 - c) multi-layered nano-graphite.
18. The insulation board of claim 17, wherein the R-value of said board is between about 3 to about 8.
19. The insulation board of claim 17, wherein said insulation board has a thickness of between about 1/8 inch to about 10 inches.
20. The insulation board of claim 19, wherein the multi-layered nano-graphite is present in an amount of from about 0.1 to about 10% by weight based on the polymer.

1/6



2/6

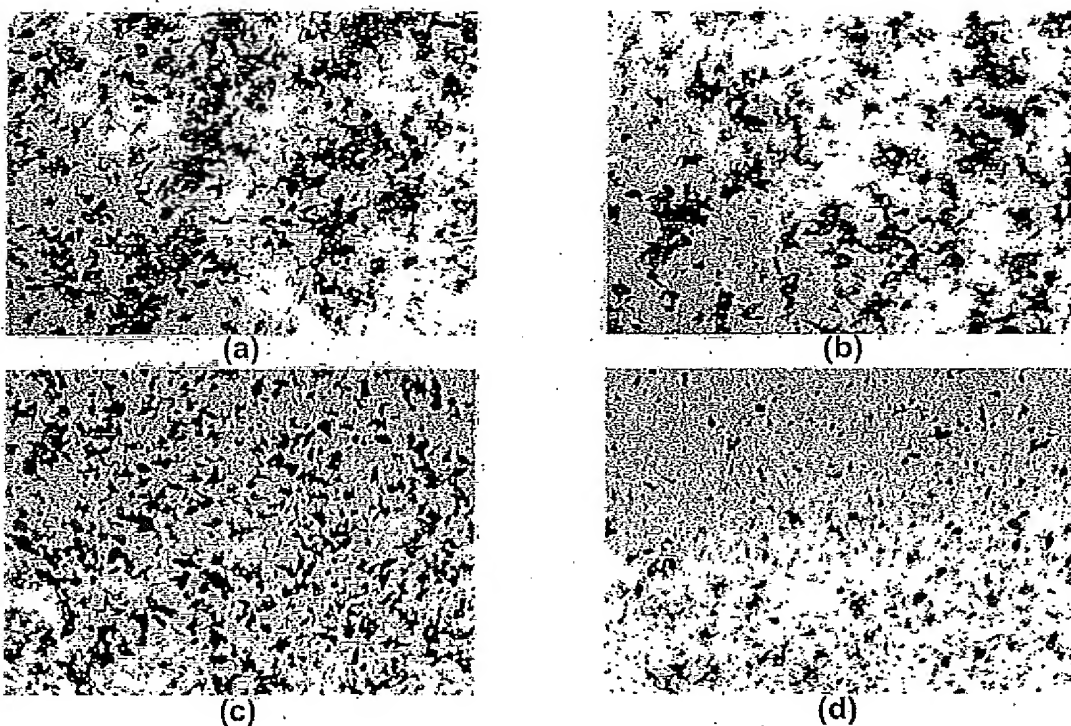
FIG. 2 Preparation of GMA-functionalized graphite



3/6

FIG. 3

Dispersion of graphite (1%) in styrene



(a) acid-treated graphite, without homogenization or ultra-sonication.

(b) acid-treated graphite, with homogenization (3 mins) and ultra-sonication (30 mins).

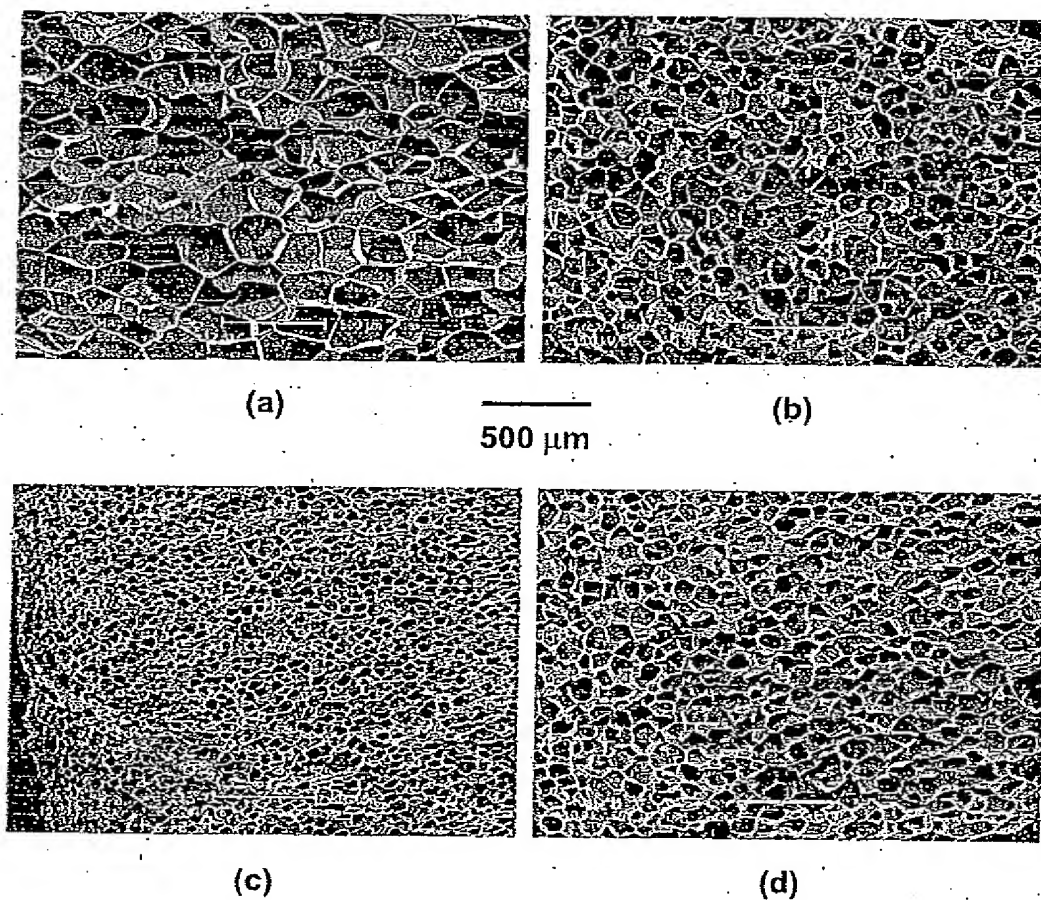
(c) GMA-functionalized graphite, without homogenization or ultra-sonication.

(d) GMA-functionalized graphite, with homogenization (3 mins) or ultra-sonication (30 mins).

4/6

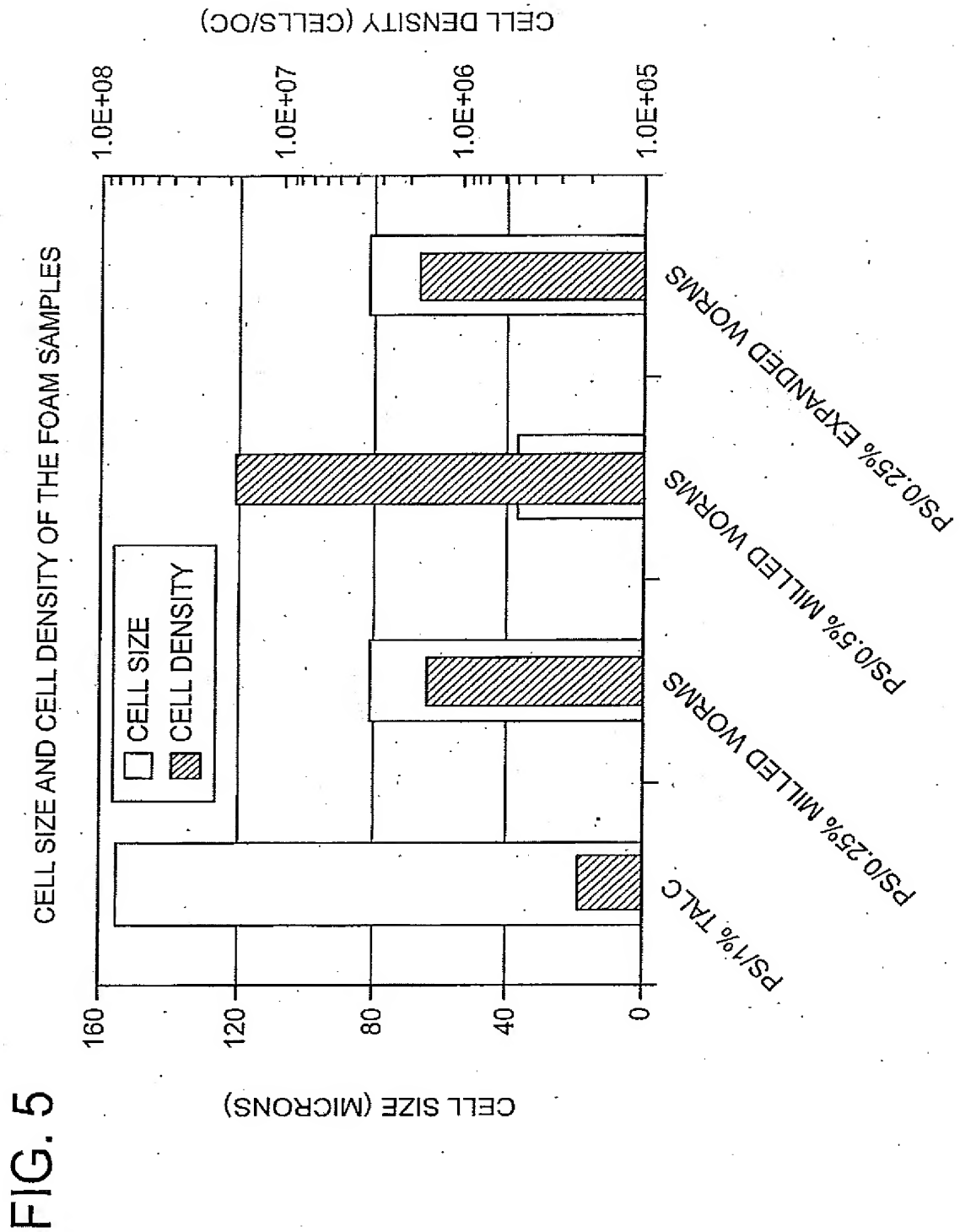
FIG. 4

Foam structure of the 4 foam samples:



- (a) PS
- (b) PS/0.25% milled worms
- (c) PS/0.5% milled worms
- (d) PS/0.25% expanded worms

5/6



6/6



50 nm

Graphite crystal in layers



5 μm

Graphite particles

FIG. 6

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2005/045291A. CLASSIFICATION OF SUBJECT MATTER
INV. C08J9/00 C08K3/04 C08J9/12

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
C08J C08K C01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 6 387 968 B1 (GLUECK GUISCARD ET AL) 14 May 2002 (2002-05-14) example 1	1-20
Y	WO 2004/065461 A (THE OHIO STATE UNIVERSITY RESEARCH FOUNDATION) 5 August 2004 (2004-08-05) page 11, paragraph 61 - page 12, paragraph 63; claims 1-36	1-20
A	EP 1 205 437 A (FUTABA CORPORATION) 15 May 2002 (2002-05-15) column 3, line 40 - line 48 paragraph [0033]	1-20
Y	WO 97/31053 A (THE DOW CHEMICAL COMPANY) 28 August 1997 (1997-08-28) claims 1-14	1-20
	----- -/--	

☒ Further documents are listed in the continuation of Box C.☒ See patent family annex.

* Special categories of cited documents:

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
- *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- * & * document member of the same patent family

Date of the actual completion of the international search

12 May 2006

Date of mailing of the international search report

22/05/2006

Name and mailing address of the ISA/

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Scheuer, S

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2005/045291

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 679 718 A (SUH ET AL)	1-20
Y	21 October 1997 (1997-10-21) column 4, line 29 - line 62; claims 1-25; table 5	1-20

Form PCT/ISA/210 (continuation of second sheet) (April 2005)

page 2 of 2

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No
PCT/US2005/045291

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
US 6387968	B1	14-05-2002	DE 19812856 A1 WO 9948957 A1 EP 1082382 A1	30-09-1999 30-09-1999 14-03-2001
WO 2004065461	A	05-08-2004	AU 2003302767 A1 US 2003205832 A1 US 2005004243 A1	13-08-2004 06-11-2003 06-01-2005
EP 1205437	A	15-05-2002	WO 0073206 A1 JP 3074170 B2 JP 2001048508 A US 6692718 B1	07-12-2000 07-08-2000 20-02-2001 17-02-2004
WO 9731053	A	28-08-1997	AT 209666 T AU 712100 B2 AU 2132297 A BR 9707867 A CN 1212001 A CZ 9802639 A3 DE 69708605 D1 DE 69708605 T2 EP 0882089 A1 ES 2163739 T3 JP 2000505491 T NO 983856 A PL 328459 A1 TR 9801635 T2	15-12-2001 28-10-1999 10-09-1997 27-07-1999 24-03-1999 13-01-1999 10-01-2002 01-08-2002 09-12-1998 01-02-2002 09-05-2000 21-08-1998 01-02-1999 23-11-1998
US 5679718	A	21-10-1997	US 5674916 A	07-10-1997